



# Efficient $\text{H}_2\text{O}_2$ production from urine treatment based on a self-biased $\text{WO}_3/\text{TiO}_2$ -Si PVC photoanode and a $\text{WO}_3/\text{CMK-3}$ cathode

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## ABSTRACT

Urine accounts for only 1% of municipal wastewater volume but contributes 80% of nitrogen, which has become one of the challenges for existing wastewater treatment plants. Herein, we proposed a novel approach based on a self-biased  $\text{WO}_3/\text{TiO}_2$ -Si PVC photoanode and a  $\text{WO}_3$ -modified mesoporous carbon (CMK-3) cathode ( $\text{WO}_3/\text{CMK-3}$ ) to produce significantly high-value chemical  $\text{H}_2\text{O}_2$  from urine treatment with effective total nitrogen removal. The central idea of the design is to achieve a feasible reversal of the thermodynamic trend of  $\text{O}_2$  reduction to  $\text{H}_2\text{O}_2$  from a non-spontaneous to a strongly spontaneous process by combining it with a urine treatment reaction that releases large amounts of chemical energy in the photoelectrocatalytic (PEC) system. The results indicated that the  $\text{H}_2\text{O}_2$  production was boosted remarkably by urine disposal reaction ( $5.13 \text{ mg cm}^{-2} \text{ h}^{-1}$ ) with a faradaic efficiency of 72%, and the  $\text{WO}_3/\text{CMK-3}$  cathode showed 6.1 and 2.5 times higher  $\text{H}_2\text{O}_2$  production activity than the common gas diffusion electrode and carbon felt electrode, respectively. Moreover, urine was degraded effectively into  $\text{N}_2$  with a total nitrogen removal of 91.4% within 120 min, and the kinetic constant of urine degradation was  $0.0397 \text{ min}^{-1}$ , which was 15.4 times that of the blank. The results of ESR and quenching experiments demonstrated that the amine group of urine selectively and rapidly converted into  $\text{N}_2$  by  $\text{Cl}\cdot$ . This study provides new insights into efficient urine disposal and synchronous  $\text{H}_2\text{O}_2$  production.

## 1. Introduction

Nitrogen pollution is the main source of eutrophication in water bodies [1]. Urine, as a high-concentration nitrogenous waste, contributes 80% of the urea-N and 10% of the COD, although it accounts for only 1% of the municipal wastewater volume [2–4]. The nitrogen content in the urine wastewater is severely overloaded, which is a difficult problem for wastewater treatment [5]. Many methods have been developed for urine-N treatment, which include nitrification and denitrification [6], reverse osmosis [7], and adsorption [8]. However, these methods still suffer from secondary contamination, low efficiency, high energy consumption and operational complexity [9–12]. The advanced oxidation processes driven by the photoelectrochemical method have also been used for urea treatment because of their effectiveness, operational simplicity, and environmental friendliness [13,14]. Moreover, it

is driven by electricity from renewable sources, such as solar and wind, providing a green and sustainable alternative to conventional treatment processes [15]. However, urea is rich in chemical energy and its simple oxidation is an exothermic process, which will result in a large amount of released chemical energy that cannot be recovered. Therefore, how to design systems for recovering chemical energy directly from urine treatment is extremely attractive [16,17].

Recently, hydrogen generation by electrolysis of urine wastewater has attracted wide attention. Since the oxidation of urea to produce  $\text{H}_2$  requires a lower potential (0.37 V) compared to water splitting, this process can significantly reduce the thermodynamic difficulties of hydrogen production, which can significantly reduce energy consumption [18,19]. Moreover, urea is an abundant source of hydrogen (~6.71 wt%), which means that the hydrogen energy in it can be efficiently recovered [20,21]. However, the process of Eq. (1) remains a

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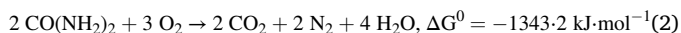
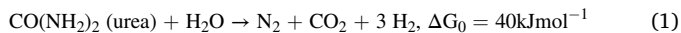
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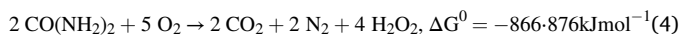
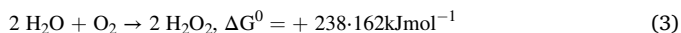
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thermodynamically non-spontaneous tendency, which requires additional energy, thus limiting the development of urine wastewater electrolysis. In terms of thermodynamics (Eq. (2)), the decomposition of urea in  $O_2$  can release a large amount of chemical energy ( $1343.2 \text{ kJ}\cdot\text{mol}^{-1}$ ), which means that urine is a rich reservoir of energy.



In addition, urea oxidation reaction (UOR) involves complicated  $6e^-$  transfer and is prone to excessive oxidation to nitrate and nitrite, leading to incomplete denitrification and secondary contamination [22]. Fortunately, recent studies have proposed to use the characteristics of high selectivity and strong oxidation of chlorine radicals ( $\text{Cl}\cdot$ ,  $\text{ClO}\cdot$ ) [23–25] to oxidize the electron-rich amine (ammonia)-nitrogen groups, which aimed to achieve simultaneous chemical energy recovery from the urine treatment process in the photoelectrochemical system and obtained satisfactory results [26,27]. On this basis, a novel electrochemical system mediated by  $\text{Cl}\cdot$  is constructed, where  $\text{Cl}\cdot$  is used as an electron mediator for the oxidative denitrogenation of urea.

Hydrogen peroxide ( $\text{H}_2\text{O}_2$ ), as a well-known green and environmentally friendly water treatment agent [28,29], which is widely used in the chemical, food, and pharmaceutical industries. In recent years, a series of  $\text{H}_2\text{O}_2$  preparation methods have been developed, among which the most studied is the oxygen reduction method. However, the  $\text{H}_2\text{O}_2$  production by oxygen reduction is a thermodynamically non-spontaneous process, which is highly energy intensive [30]. For this reason, we imagine that if the urine oxidative denitration process can combine with the  $\text{H}_2\text{O}_2$  preparation process, i.e., Eq. (2) + Eq. (3), a new chemical reaction can be formed (Eq. (4)), which is a process with a strong thermodynamic spontaneous trend. This means that the chemical energy released from urine disposal can be effectively recovered by the reduction of  $O_2$  to produce  $\text{H}_2\text{O}_2$ .



Based on the above consideration, we presented a novel method based on a self-biased  $\text{WO}_3/\text{TiO}_2\text{-Si PVC}$  photoanode and a  $\text{WO}_3/\text{CMK-3}$  cathode to significantly produce the high value-added chemical  $\text{H}_2\text{O}_2$  from urine treatment with efficient total nitrogen removal. A  $\text{WO}_3$ -modified mesoporous carbon electrode ( $\text{WO}_3/\text{CMK-3}$ ) served as the cathode on account of its high specific surface area and hydrophilic/hydrophobic interface, which can give it a large number of catalytic active sites and efficient  $O_2$  transfer channels for efficient  $\text{H}_2\text{O}_2$  production. A self-biased composite photoanode was employed as the anode ( $\text{WO}_3/\text{TiO}_2\text{-Si PVC}$ ) to strengthen the generation of  $\text{Cl}\cdot$  for highly selective removal of total nitrogen from urine, which was constituted by front  $\text{WO}_3/\text{TiO}_2$  photoanode and rear polycrystalline silicon cell (Si PVC). Electrons generated from the oxidation of urine were then transported to the cathode for  $\text{H}_2\text{O}_2$  production. We first investigated the  $\text{H}_2\text{O}_2$  production performance of the  $\text{WO}_3/\text{CMK-3}$  cathode and then evaluated the  $\text{H}_2\text{O}_2$  production from synthetic urine treatment. Meanwhile, the total nitrogen removal efficiencies of synthetic urine and actual urine were also been assessed. ESR analysis and quenching experiments were performed to investigate the mechanism of  $\text{Cl}\cdot$  production for urine degradation. This work offers new perspectives on effective urine treatment and synchronous  $\text{H}_2\text{O}_2$  generation.

## 2. Experimental

### 2.1. Chemicals and materials

Mesoporous carbon CMK-3 was purchased from XFNANO (Nanjing, China). Nafion 117 membrane and Nafion dispersions were purchased from Dupont. Carbon paper material (CP) was obtained from Keqi

(Shanghai, China). Other chemical reagents of analytical grade used in the study were obtained from Macklin. Deionized water ( $\text{DI}, \geq 18.25 \text{ M}\Omega\cdot\text{cm}$ ) was utilized for the preparation/dilution of all samples.

### 2.2. Fabrication of the $\text{WO}_3/\text{CMK-3}$ cathode

Firstly, the  $\text{WO}_3$  nanoparticle supported on mesoporous carbon CMK-3 was prepared by the polymeric precursor method (PPM) [31], in which tungsten chloride was used to find the best tungsten proportion. Then, the  $\text{WO}_3$ -loaded CMK-3 catalyst was spray-coated on the commercial CP to obtain a catalytic layer ( $0.653 \text{ mg cm}^{-2}$ ). The schematic diagram of the fabrication process of the  $\text{WO}_3/\text{CMK-3}$  cathode was shown in Fig. S1. The CP was immersed in PTFE suspension (2%, v/v) for 10 min, dried in the oven, and then calcined at  $360^\circ\text{C}$  for 0.5 h to form a super-hydrophobic gas diffusion layer. A catalyst suspension containing 20 mg CMK-3, 125  $\mu\text{L}$  Nafion solution (5 wt%), 5 mL ethanol, and 1 mL DI water was sequentially homogenized by stirring and ultrasonic treatment for 1 h. Then, 2 mL of the homogenized suspension was spray-coated on the CP and dried at room temperature. After calcining at  $360^\circ\text{C}$  for 0.5 h, the  $\text{WO}_3/\text{CMK-3}$  cathode was obtained ( $1 \times 1 \text{ cm}^2$ ).

### 2.3. Construction of the $\text{WO}_3/\text{TiO}_2\text{-Si PVC}$ photoanode

The  $\text{WO}_3/\text{TiO}_2$  nanoplate photoanode was fabricated by a hydrothermal synthesis method [32,33], and the detailed procedure was shown in Fig. S2. A commercial silicon photovoltaic cell pack (Si PVC,  $3.7 \times 6.8 \text{ cm}^2$ ) connected in series by copper strip and Ag epoxy was used as the rear photoanode. The positive pole of Si PVC was connected to the back of the  $\text{WO}_3/\text{TiO}_2$  photoanode by copper wire and then sealed via silicone rubber to form a composite photoanode. The illustration of the  $\text{WO}_3/\text{TiO}_2\text{-Si PVC}$  photoanode in the PEC system was displayed in Fig. S3.

### 2.4. Experimental setup

As shown in Fig. 1, the photoelectrocatalytic experiments for synthetic urine treatment and simultaneous  $\text{H}_2\text{O}_2$  generation were performed in a flow cell reactor with a two-electrode system, where  $\text{WO}_3/\text{CMK-3}$  and  $\text{WO}_3/\text{TiO}_2\text{-Si PVC}$  were used as the cathode and photoanode, respectively. A 300-W Xe lamp with an AM 1.5 filter (PerfectLight, China) was applied for light illumination ( $100 \text{ mW cm}^{-2}$ ). The reactor contains three chambers, in which the anodic chamber was fed with a solution containing  $30 \text{ mg L}^{-1}$  urea,  $0.1 \text{ M Na}_2\text{SO}_4$  and  $0.05 \text{ M NaCl}$ , the cathodic chamber was supplied with  $0.1 \text{ M Na}_2\text{SO}_4$ , and the gas chamber was flushed with continuous  $O_2$  flow. The anodic and cathodic chambers were separated by a proton exchange membrane (PEM, Nafion 117). The anolyte was circulated to evaluate the accumulated urea degradation, and the catholyte flowed in a single pass to bring out the synthesized  $\text{H}_2\text{O}_2$  at a flexible rate. All experiments were carried out in an electrochemical workstation (CHI 660c, China). Samples were taken at regular intervals to determine urea, nitrate nitrogen, ammonia nitrogen and total nitrogen in the anodic chamber and hydrogen peroxide in the cathodic chamber. The quantification of  $\text{H}_2\text{O}_2$  was carried out by the potassium titanium oxalate method [34], which was measured by a UV-vis spectrophotometer (752 N, INESA, Shanghai) at  $410 \text{ nm}$ . The actual urine wastewater was collected from the public latrines. After filtering ( $0.45 \mu\text{m}$ ) and diluting to the appropriate concentration (physicochemical properties were shown in Table S2), it was treated with the same device.

### 2.5. Analytical methods

The surface morphology and composition of electrodes were determined by high-resolution transmission electron microscopy (HRTEM, JEOL-2100 F/F200) and a scanning electron microscopy (SEM, Zeiss SUPRA55-VP) equipped with an X-ray energy dispersive spectrometer

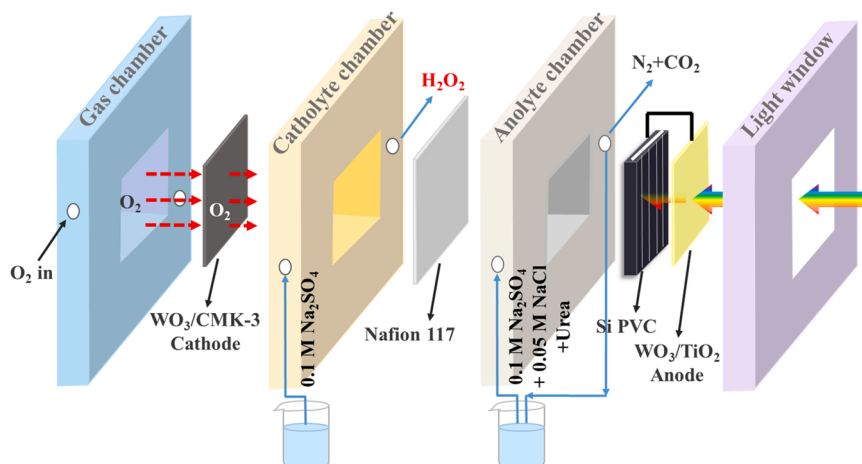


Fig. 1. Schematic illustration of the PEC system for efficient  $\text{H}_2\text{O}_2$  production from urine treatment.

(EDS). X-ray diffraction (XRD, Rigaku D-Max B) was used to measure the crystal structure of the electrodes. The elemental compositions of electrodes were analyzed with an X-ray photoelectron spectroscopy (XPS, AXIS Ultra DLD). Brunauer–Emmett–Teller (BET) surface area and pore-size distributions were measured using  $\text{N}_2$  adsorption–desorption isotherms (Autosorb-iQ/ASAP 2460). The Fourier transform infrared (FT-IR) spectra were collected on a Thermo Nicolet 6700 spectrometer (U. S.). The contact angle of the sample was characterized with a drop shape analyzer (KRUS, Germany, DSA100). Linear sweep voltammetry (LSV) and cyclic voltammetry (CV) were performed in a three-electrode system at a scan rate of  $50 \text{ mV s}^{-1}$  in  $0.1 \text{ M Na}_2\text{SO}_4$  solution. The free radical species were determined using the electron spin resonance method (ESR, LP920).

The rotation ring disk electrode (RRDE) tests were performed in a typical three-electrode cell with a reference electrode of  $\text{Ag}/\text{AgCl}$ . A RRDE assembly (AFMSRCE, Pine Instruments) consisting of a glassy carbon rotating disk electrode (area =  $0.2472 \text{ cm}^2$ ) and a Pt ring (area =  $0.1859 \text{ cm}^2$ ) was used as a working electrode with a theoretical collection efficiency of  $N = 0.389$ . To prepare the working electrode, a solution containing  $10 \text{ mg}$  of catalyst was mixed with  $3 \text{ mL}$  of isopropanol and  $30 \mu\text{L}$  of Nafion 117 solution and sonicated for  $20 \text{ min}$  to obtain a homogeneous catalyst ink, and then  $6 \mu\text{L}$  of the ink was painted onto the glassy carbon disk to obtain a catalyst loading of  $0.08 \text{ mg cm}^{-2}$ . The  $\text{H}_2\text{O}_2$  molar selectivity can be calculated by the following equation:

$$\text{H}_2\text{O}_2 \text{ molar selectivity} = \frac{i_r/N}{i_r/N + i_d} \times 200$$

where  $i_r$  and  $i_d$  represent the ring current and disk current (mA), respectively.

Urea concentration was determined by high-performance liquid chromatography (HPLC-2010 Plus, Shimadzu). The concentration of ammonia nitrogen was determined by Nessler's reagent colorimetric method, and the absorbance at  $420 \text{ nm}$  was measured using a UV–vis spectrophotometer (TU-1901, Pgeneral). Nitrate and nitrite were determined using ion chromatography (ICS-5000 +/900). TN was determined using a TN/TOC analyzer (Analytik Jena). The generated  $\text{N}_2$  was analyzed by a gas chromatograph (GC9790 Plus, China).

### 3. Results and discussion

#### 3.1. Characterization of the electrodes

To realize efficient mass transfer and catalytic reduction of  $\text{O}_2$ , a novel gas diffusion cathode with the hydrophilic/hydrophobic interface was designed ( $\text{WO}_3/\text{CMK-3}$ ). The  $\text{WO}_3/\text{CMK-3}$  cathode was composed of a gas diffusion layer and a catalytic layer, and the preparation process

was illustrated in Fig. S1. Carbon paper was used as the gas diffusion layer because of its abundant macropore and microporous structure (Fig. S4), which endows it with fast gas permeation and low gas diffusion resistance. To prevent carbon paper from water flooding and further improve its oxygen diffusion performance, the superhydrophobic modification of carbon paper using PTFE was performed. And the water contact angle measurement results showed that the PTFE-modified CP exhibited prominent hydrophobicity with a water CA of  $143^\circ$  (Fig. S5 (a)). Mesoporous carbon CMK-3 was used as the catalyst substrate due to its large BET surface area, abundant defect active sites, and positive zeta potential, which endows it with excellent selectivity for  $\text{H}_2\text{O}_2$  production [35,36]. To further strengthen the catalytic activity of CMK-3 for  $\text{H}_2\text{O}_2$  production, the  $\text{WO}_3$  modification on CMK-3 proceeded owing to its loading on CMK-3 may improve the activity and selectivity by introducing a large number of oxygen-containing functional groups and increasing the hydrophilicity of the catalyst surface [31,37]. The CA results (Fig. S5(b)) confirmed the excellent hydrophilicity of the catalytic layer ( $88.8^\circ$ ). The surface morphology of the  $\text{WO}_3$ -modified CMK-3 cathode is displayed in Fig. 2(a), which exhibits a loose skeleton and a hierarchical porous structure. The EDS mappings of the  $\text{WO}_3/\text{CMK-3}$  cathode are shown in Fig. 2(b), which illustrates the existence and uniform dispersion of C, O and W on the selected architecture. The TEM images show that  $\text{WO}_3$  is uniformly dispersed on CMK-3 (Fig. 2(c)), and a lattice fringe of  $0.388 \text{ nm}$  is clearly observed (Fig. 2(d)), corresponding to the (002) crystal plane of  $\text{WO}_3$ . With the increase of the  $\text{WO}_3$  modification ratio, the more obvious  $\text{WO}_3$  agglomeration (Fig. S6(a)–(d)). The XRD patterns of the  $\text{WO}_3/\text{CMK-3}$  cathodes with different W proportions (w/w) are displayed in Fig. 2(e), clearly showing the characteristic peaks at  $2\theta = 23.1, 23.6, \text{ and } 24.4^\circ$ , corresponding to the (002), (020) and (200) crystalline planes of  $\text{WO}_3$ , respectively. This indicated that the  $\text{WO}_3$  was successfully modified on CMK-3 according to JCPDF #20–1323. To further investigate the structure and porosity of different  $\text{WO}_3$ -modified catalysts, the adsorption–desorption isotherms of  $\text{N}_2$  were analyzed. As depicted in Fig. 2(f), the isotherms were all type IV, which confirmed the coexistence of micropores, mesopores, and macropores. As the amount of  $\text{WO}_3$  increased, the BET surface areas decreased from  $1297.71$  to  $689.98 \text{ m}^2 \text{ g}^{-1}$ , and the pore volume decreased from  $2.66$  to  $1.46 \text{ cm}^3 \text{ g}^{-1}$  (Table S1), which may be ascribed to the formation of  $\text{WO}_3$  nanoparticles on CMK-3 pores. Micropores provide active sites for oxygen reduction reaction (ORR), but mesopores and macropores serve as gas transfer channels to supply oxygen [38]. Besides, it can be observed that the  $\text{WO}_3$  modification did not change the morphology and size of CMK-3 (Fig. S7). These results indicated that the large BET surface area and abundant pore structure give the  $\text{WO}_3$ -modified CMK-3 a large number of exposed catalytic sites, which is conducive to the reduction of  $\text{O}_2$  to produce  $\text{H}_2\text{O}_2$  [39].



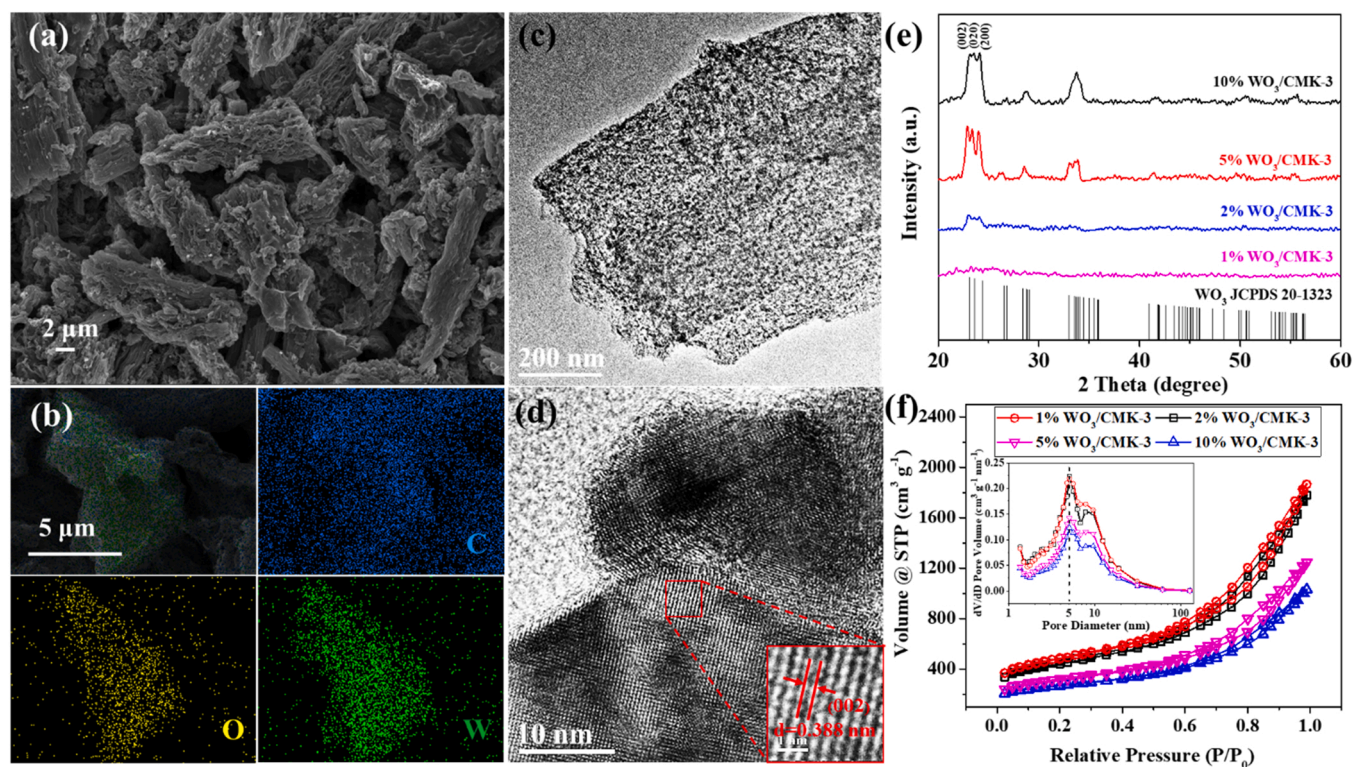


Fig. 2. SEM image of (a)  $\text{WO}_3/\text{CMK-3}$  cathode. (b) EDS elemental mappings of C, O, and W. (c)-(d) TEM images of  $\text{WO}_3/\text{CMK-3}$  at different magnifications. (e) XRD patterns of  $\text{WO}_3/\text{CMK-3}$  catalysts with different W proportions (w/w). (f)  $\text{N}_2$  adsorption-desorption isotherms and pore-size distribution (inset) of catalytic layer materials with different W proportions (w/w).

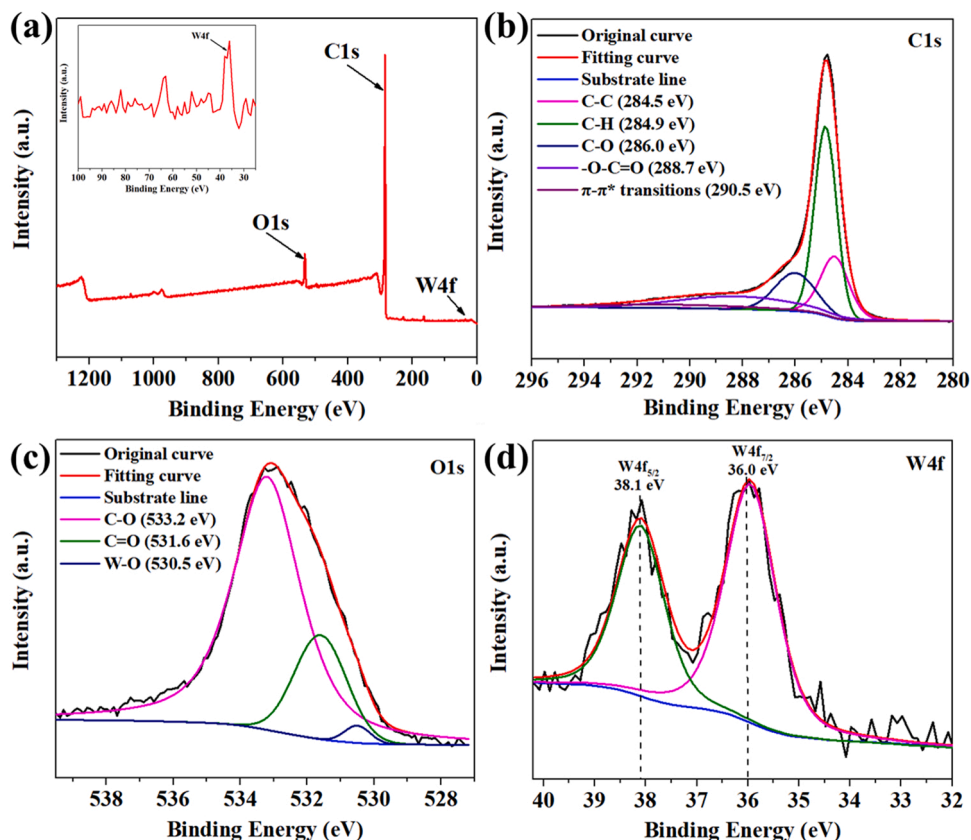


Fig. 3. (a) XPS spectra of  $\text{WO}_3/\text{CMK-3}$  cathode. Deconvoluted (b) C 1s, (c) O 1s, and (d) W 4f spectra of  $\text{WO}_3/\text{CMK-3}$  cathode.



XPS was used to investigate the surface elemental compositions and chemical bonding states of the  $\text{WO}_3/\text{CMK-3}$  cathode. The survey spectra demonstrated the strong peaks assigned to C 1 s, O 1 s, and W 4 f, further indicating the successful modification of W on the CMK-3 catalyst (Fig. 3(a)). The C 1 s spectra of the  $\text{WO}_3/\text{CMK-3}$  (Fig. 3(b)) can be deconvoluted into the following bands: graphite carbon (C-C) at 284.5 eV, C-H bond at 284.9 eV, C-O bond at 286.0 eV, carboxyl O-C=O at 288.7 eV and the characteristic shakeup line of carbon at 290.5 eV ( $\pi-\pi^*$  transition) [37]. The deconvolution of the O 1 s spectra (Fig. 3(c)) showed four independent peaks: oxygen singly bound to carbon (C-O) at 533.2 eV, oxygen doubly bound to carbon (C=O) at 531.6 eV and W-O bond (derived from  $\text{WO}_3$  modified on CMK-3) at 530.5 eV. In the W 4 f region (Fig. 3(d)), the spectra had two independent peaks at 36.0 eV and 38.1 eV, and the interval is 2.1 eV, which is consistent with the standard spectra of  $\text{WO}_3$ . In addition, Fig. S8 depicts the XPS survey scans of CMK-3 modified with and without  $\text{WO}_3$ , which exhibited a significant enhancement in the oxygen content of  $\text{WO}_3$ -modified CMK-3. These results confirmed that the  $\text{WO}_3$  modification induced more oxygenated

functional groups (such as C-OH, C=O, and C-OOH, etc.), which could be further demonstrated by the FT-IR results in Fig. S9).

The morphology of the synthesized  $\text{WO}_3/\text{TiO}_2$  photoanode was displayed in Fig. 4. As shown in the SEM results,  $\text{WO}_3$  and  $\text{WO}_3/\text{TiO}_2$  exhibited staggered plate-like structure (Fig. 4(a)-(d)), and  $\text{TiO}_2$  was epitaxially grown on the surface of  $\text{WO}_3$  in the form of nanoprickle. Besides, the EDS mappings shown in Fig. 4(e) demonstrated the existence and uniform dispersion of W, O and Ti on the selected architecture. High-resolution transmission electron microscopy (HRTEM) image of  $\text{WO}_3/\text{TiO}_2$  show that the thickness of the  $\text{TiO}_2$  nanoprickle overlayer is  $\sim 50$  nm (Fig. 4(f)), and a typical lattice fringe spacing of 0.238 nm is observed (Fig. 4(g)), corresponding to the (004) crystal plane of anatase  $\text{TiO}_2$  [32,40]. The XPS spectra results of  $\text{WO}_3/\text{TiO}_2$  showed two characteristic peaks of anatase at 459.2 and 465.0 eV (as shown in Fig. S10), which further confirmed the successful modification of  $\text{TiO}_2$  on  $\text{WO}_3$ . In addition, the XRD results suggested that  $\text{WO}_3$  primarily grew on the FTO substrate in the form of a triclinic crystalline phase, and  $\text{TiO}_2$  grew on  $\text{WO}_3$  in the form of anatase with a characteristic peak of  $25.3^\circ$  (Fig. 4

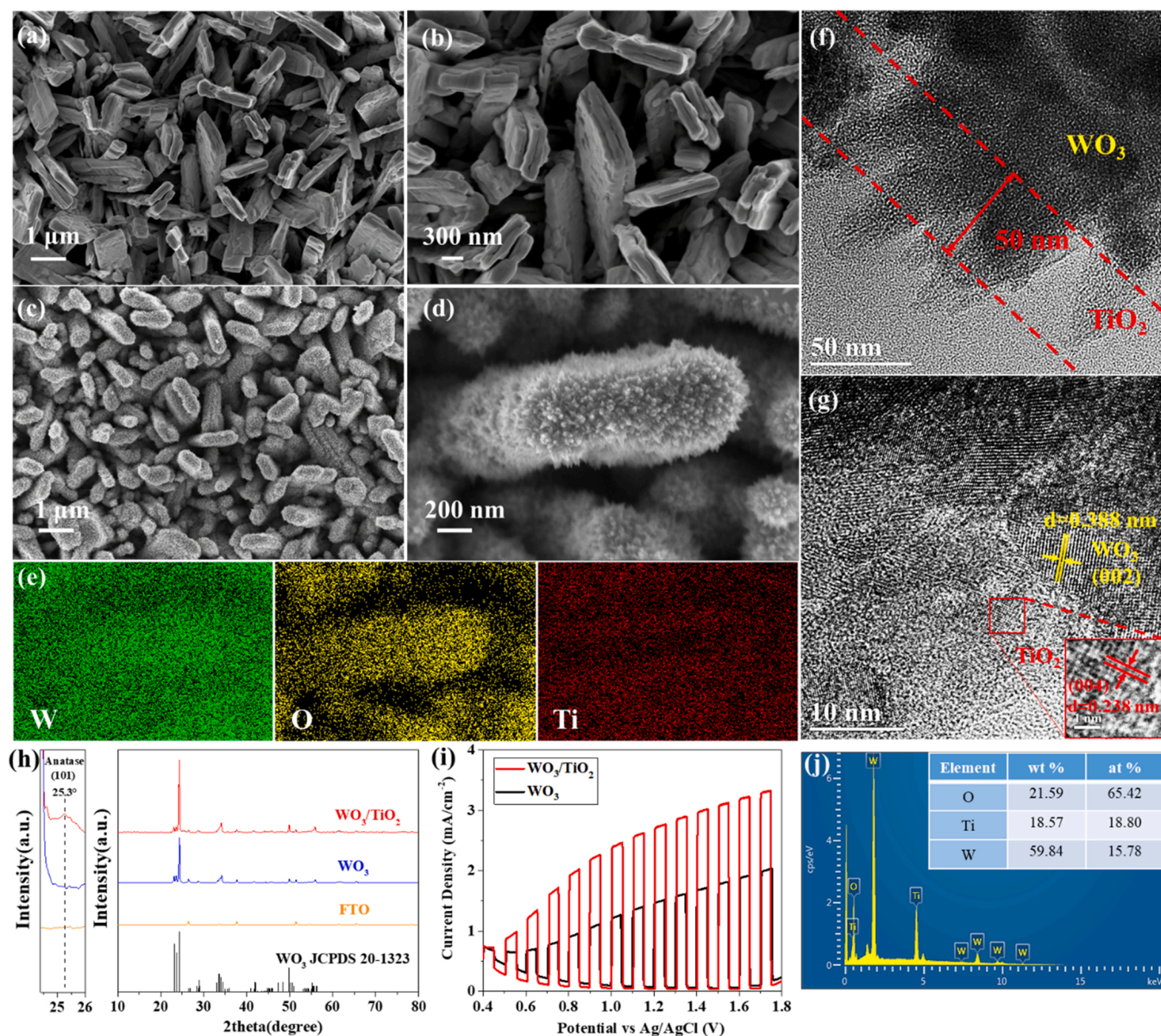


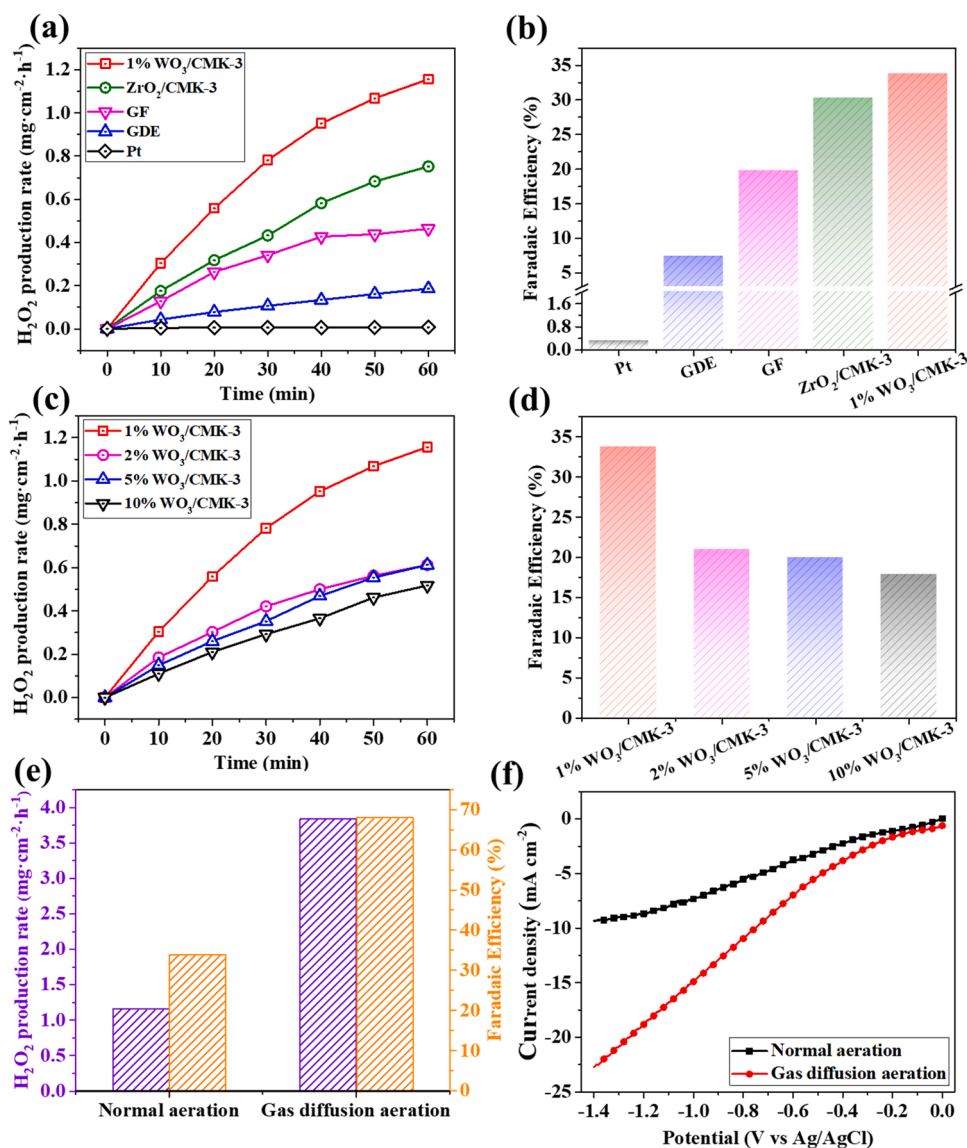
Fig. 4. SEM images of (a)-(b)  $\text{WO}_3$  and (c)-(d)  $\text{WO}_3/\text{TiO}_2$  electrodes at different magnifications. (e) EDS elemental mappings of W, O and Ti. (f)-(g) HRTEM image of  $\text{WO}_3/\text{TiO}_2$  electrodes. (h) XRD patterns and (i) chopped J-V curves (scan rate  $5 \text{ mV s}^{-1}$ ) of  $\text{WO}_3$  and  $\text{WO}_3/\text{TiO}_2$  electrodes. (j) EDS atomic ratio of W, O and Ti  $\text{WO}_3/\text{TiO}_2$  electrode.

(h)). To assess the PEC performance of the photoanodes, the chopped photocurrent-potential (J-V) plots of  $\text{WO}_3$  and  $\text{WO}_3/\text{TiO}_2$  photoanodes have been investigated under AM 1.5 light ( $100 \text{ mW cm}^{-2}$ ) irradiation (Fig. 4(i)). The results showed that  $\text{WO}_3/\text{TiO}_2$  electrode possesses an excellent photocurrent density of  $\sim 1.86 \text{ mA cm}^{-2}$  at 1.23 V vs. RHE (reversible hydrogen electrode), which is 2.07 times of the  $\text{WO}_3$  electrode ( $\sim 0.9 \text{ mA cm}^{-2}$ ). This indicated that the  $\text{WO}_3/\text{TiO}_2$  photoanode has better charge separation and collection performance, which can be ascribed to multiple factors. Firstly, the type-II heterojunction interfacial band structure of  $\text{WO}_3/\text{TiO}_2$  photoanode reduces the possibility of surface trap recombination and improves the separation of electron-hole pairs. Meanwhile, the feature that  $\text{TiO}_2$  can absorb UV light also ensures its enhanced charge transport properties for  $\text{WO}_3$  by generating charge carriers [41,42]. Moreover, the large surface curvatures of the  $\text{TiO}_2$  nanoprickle can significantly strengthen its local electric field, and then selectively transfer the hole to the nanoprickle end. The coverage of  $\text{TiO}_2$  can also hinder the formation of peroxotungstate on the  $\text{WO}_3$  surface and prevent the passivation of  $\text{WO}_3$ , and then enhance the charge transfer at its interface with the electrolyte [32]. In addition, stability tests of the photoanodes were performed at different pH

conditions. The results showed that  $\text{TiO}_2/\text{WO}_3$  was superior to  $\text{WO}_3$  alone (Fig. S11), which may be due to the modification of  $\text{TiO}_2$  can completely seal the surface of  $\text{WO}_3$ , thus greatly improving the corrosion resistance of the anodes [43]. All these results indicated the superiority of  $\text{WO}_3/\text{TiO}_2$  over  $\text{WO}_3$  photoanode, which can adapt to stricter reaction conditions.

### 3.2. Hydrogen peroxide production

As mentioned above, we have constructed a novel photoelectrocatalytic system with self-biased  $\text{WO}_3/\text{TiO}_2\text{-Si}$  PVC as photoanode and  $\text{WO}_3/\text{CMK-3}$  as cathode, which is used to produce  $\text{H}_2\text{O}_2$  from synergistic urine treatment. To investigate the efficiency of  $\text{H}_2\text{O}_2$  synthesis on the  $\text{WO}_3/\text{CMK-3}$  cathode in this system, the yield of  $\text{H}_2\text{O}_2$  and faradaic efficiency (FE) were assessed. As shown in Fig. S12(a), the  $\text{WO}_3/\text{CMK-3}$  cathode showed a significantly high  $\text{H}_2\text{O}_2$  yield of  $1.16 \text{ mg cm}^{-2} \text{ h}^{-1}$  under the normal aeration ( $\text{O}_2$  diffused through the electrolyte), which is much higher than that of the CP ( $0.38 \text{ mg cm}^{-2} \text{ h}^{-1}$ ) and CMK-3 cathode ( $0.53 \text{ mg cm}^{-2} \text{ h}^{-1}$ ). In addition, the FE of the  $\text{WO}_3/\text{CMK-3}$  cathode reached 33.8%, which was 17.6% and 11.8%



**Fig. 5.** (a)  $\text{H}_2\text{O}_2$  yield and (b) Faradaic efficiency of different cathodes; (c)  $\text{H}_2\text{O}_2$  yield and (d) Faradaic efficiency of  $\text{WO}_3/\text{CMK-3}$  cathodes with different W proportions (w/w); Conditions : pH= 2, 0.1 M  $\text{Na}_2\text{SO}_4$ , normal aeration. Effects of (e) aeration modes on  $\text{H}_2\text{O}_2$  yield, Faradaic efficiency, and (f) current density of 1%  $\text{WO}_3/\text{CMK-3}$  cathode. Conditions: pH= 2, 0.1 M  $\text{Na}_2\text{SO}_4$ , gas diffusion aeration.



higher than that of the CP (16.2%) and CMK-3 cathode (22.0%), respectively (Fig. S12(b)). We then monitored the current and found the largest value for the WO<sub>3</sub>/CMK-3 cathode (Fig. S12(c)), corresponding to its best H<sub>2</sub>O<sub>2</sub> production performance. A comparison of the performance of similar PEC systems for photocatalytic production of H<sub>2</sub>O<sub>2</sub> has been summarized in Table S3. Compared with the PEC systems in other studies, the WO<sub>3</sub>/CMK-3 cathode of our system proposed in this study exhibited significant superiority in H<sub>2</sub>O<sub>2</sub> generation. In addition, the current response of the prepared cathodes was significantly enhanced, indicating that the catalytic activity of H<sub>2</sub>O<sub>2</sub> production was improved by incorporating the WO<sub>3</sub> into the CMK-3 surface. As analyzed by XPS and FT-IR results, WO<sub>3</sub> modification can form a large number of oxygen-containing functional groups on the CMK-3 surface, thus increasing the catalytic activity for H<sub>2</sub>O<sub>2</sub> production [37]. Moreover, due to the presence of Lewis and Brønsted acid sites associated with W<sup>6+</sup> species, the modification of WO<sub>3</sub> can make the catalyst surface exhibit acidity, and then exhibit a higher affinity for species with OH<sup>-</sup>, which in turn provide more hydrophilicity and then accelerate the formation of the gas-liquid-solid three-phase interface [44]. The hydrophilic modifications can not only promote the transfer of reactants (H<sup>+</sup>) and products (H<sub>2</sub>O<sub>2</sub>) on the catalyst interface [45], but also favor the adsorption of O<sub>2</sub> according to the Pauling model, which can greatly improve the selectivity of H<sub>2</sub>O<sub>2</sub> generation [44].

The H<sub>2</sub>O<sub>2</sub> generation activity on WO<sub>3</sub>/CMK-3 cathode was also compared with ZrO<sub>2</sub>/CMK-3, graphite felt (GF), common gas diffusion electrode (GDE) and Pt. As depicted in Fig. 5(a), the WO<sub>3</sub>/CMK-3 cathode exhibited the best H<sub>2</sub>O<sub>2</sub> generation performance (1.16 mg cm<sup>-2</sup> h<sup>-1</sup>), which was 1.6, 2.5 and 6.1 times than that of the ZrO<sub>2</sub>/CMK-3 (0.75 mg cm<sup>-2</sup> h<sup>-1</sup>), GF (0.46 mg cm<sup>-2</sup> h<sup>-1</sup>) and GDE (0.19 mg cm<sup>-2</sup> h<sup>-1</sup>), respectively. However, the H<sub>2</sub>O<sub>2</sub> yield on Pt was negligible (0.01 mg cm<sup>-2</sup> h<sup>-1</sup>). In addition, Fig. 5(b) showed that the WO<sub>3</sub>/CMK-3 cathode presented the highest Faradaic efficiency of 33.8%, while the ZrO<sub>2</sub>/CMK-3, GF, GDE, and Pt cathode corresponded to 30.3%, 19.8%, 7.4%, and 0.3%, respectively. All these results demonstrated that the WO<sub>3</sub>/CMK-3 cathode possesses the outstanding performance of H<sub>2</sub>O<sub>2</sub> generation, which could be attributed not only to the ordered mesoporous structure of CMK-3 ensuring abundant catalytic active sites and potential scalability toward H<sub>2</sub>O<sub>2</sub> generation but also to the hydrophilic modification of CMK-3 using WO<sub>3</sub> ensuring excellent two-electron ORR selectivity.

To explore the optimal W ratio in WO<sub>3</sub>/CMK-3 cathodes for H<sub>2</sub>O<sub>2</sub> production, a series of experiments were conducted. As shown in Fig. 5(c), the highest H<sub>2</sub>O<sub>2</sub> production rate (1.16 mg cm<sup>-2</sup> h<sup>-1</sup>) was achieved for 1% WO<sub>3</sub>/CMK-3 cathode. As the proportion of W increased, the H<sub>2</sub>O<sub>2</sub> production rate significantly decreased. In the comparison of Faradaic efficiency (Fig. 5(d)), the 1% WO<sub>3</sub>/CMK-3 cathode was also the highest (33.8%), and this trend was consistent with the H<sub>2</sub>O<sub>2</sub> production. These results can be attributed to the decrease in specific surface area and pore volume of the catalytic layer due to the increased amount of WO<sub>3</sub> (Fig. 2(f) and Table S1), resulting in a decline in the active sites and O<sub>2</sub> transport channels. Moreover, as mentioned in the work of S.N. Eroglu, the excessive addition of WO<sub>3</sub> may lead to the degradation of peroxides, which may be another reason for the lower H<sub>2</sub>O<sub>2</sub> yield of CMK-3 at higher WO<sub>3</sub> loading [46]. In addition, it has also demonstrated that lower content of metal loading on carbon catalysts is more active for hydrogen peroxide generation [47]. To further compare the intrinsic 2e<sup>-</sup>-ORR performance of carbon catalysts with different W proportions (w/w), RRDE tests were carried out in 0.1 M Na<sub>2</sub>SO<sub>4</sub> solution. The catalyst was homogeneously coated on a glassy carbon disc electrode with a mass loading of 0.08 mg cm<sup>-2</sup>. The electrolyte solution was pre-saturated with O<sub>2</sub> before each test. To allow efficient H<sub>2</sub>O<sub>2</sub> diffusion into the Pt ring and to minimize H<sub>2</sub>O<sub>2</sub> decomposition, the rotational speed was fixed at 1600 rpm. As shown in Fig. S13(a), among all of the catalysts studied, the 1% WO<sub>3</sub>/CMK-3 exhibited the highest ring current, which corresponds to the best activity and selectivity for H<sub>2</sub>O<sub>2</sub> production (Fig. S13(b)). Such trend in RRDE indicate a higher H<sub>2</sub>O<sub>2</sub>

yield for 1% WO<sub>3</sub>/CMK-3, which is consistent with the previous TEM and BET analysis results.

As the electrode can only capture dissolved oxygen in an aqueous solution under normal aeration, and the O<sub>2</sub> solubility in an aqueous solution is very low (about 8 mg L<sup>-1</sup> at ambient temperature and pressure), the reduction reaction of O<sub>2</sub> on the electrode surface will be greatly limited by oxygen transfer. Once the optimal cathode catalyst for H<sub>2</sub>O<sub>2</sub> generation was determined, the investigation of the effect of gas diffusion modes on H<sub>2</sub>O<sub>2</sub> production was highly necessary. Fig. 5(e) compared the H<sub>2</sub>O<sub>2</sub> yield and Faradaic efficiency of the 1% WO<sub>3</sub>/CMK-3 cathode for the photoelectrocatalytic system in different aeration modes. As the results showed, the H<sub>2</sub>O<sub>2</sub> yield of 1% WO<sub>3</sub>/CMK-3 cathode reached 3.84 mg cm<sup>-2</sup> h<sup>-1</sup> in gas diffusion aeration, which was 3.3 times that in normal aeration. The Faradaic efficiency of the as-prepared cathode achieved 68% in gas diffusion aeration, which was 34.2% higher than that in normal aeration. Subsequently, the current of the as-prepared cathode was monitored in different aeration modes (Fig. 5(f)), which showed that the current was significantly higher in gas diffusion aeration, corresponding to its higher H<sub>2</sub>O<sub>2</sub> production performance.

Since the refresh of the electrolyte can immediately replenish H<sup>+</sup> and transfer the generated H<sub>2</sub>O<sub>2</sub>, and then facilitating the oxygen reduction reaction to produce H<sub>2</sub>O<sub>2</sub>, the exploration of the effect of electrolyte flow rate on H<sub>2</sub>O<sub>2</sub> production was significant. As displayed in Fig. S14(a), the H<sub>2</sub>O<sub>2</sub> production rate increased from 2.18 to 3.84 mg cm<sup>-2</sup> h<sup>-1</sup> as the electrolyte flow rate varied from 2 to 10 mL min<sup>-1</sup>, and the Faradaic efficiency increased from 41% to 70%, which were consistent with the expected results. As oxygen mass transfer at the cathodic reaction interface is an important factor for achieving efficient H<sub>2</sub>O<sub>2</sub> production [48], the influence of the O<sub>2</sub> flow rate on H<sub>2</sub>O<sub>2</sub> production was investigated. The results showed that both the H<sub>2</sub>O<sub>2</sub> production rate and the Faradaic efficiency increased as the O<sub>2</sub> flow rate increased from 20 to 100 mL min<sup>-1</sup> (Fig. S14(b)), confirming the significant effect of mass transfer of oxygen on the H<sub>2</sub>O<sub>2</sub> production. In addition, the effect of the initial solution pH on the H<sub>2</sub>O<sub>2</sub> production was tested. As depicted in Fig. S14(c), the H<sub>2</sub>O<sub>2</sub> production rate of 1% WO<sub>3</sub>/CMK-3 cathode increased from 2.46 to 3.84 mg cm<sup>-2</sup> h<sup>-1</sup> as the solution pH decreased from 8 to 2. High H<sub>2</sub>O<sub>2</sub> yields were obtained on the cathode with low pH, which can be explained by the participation of H<sup>+</sup> in H<sub>2</sub>O<sub>2</sub> generation and H<sub>2</sub>O<sub>2</sub> decomposition at alkaline pH (2 H<sub>2</sub>O<sub>2</sub> → 2 H<sub>2</sub>O + O<sub>2</sub>). In addition, the W dissolution in the WO<sub>3</sub>/CMK-3 cathode during operation (pH=8) may be another reason, as analyzed by Inductively Coupled Plasma Optical-Emission Spectroscopy (ICP-OES) in Fig. S15. Notably, the Faradaic efficiency of WO<sub>3</sub>/CMK-3 cathode does not vary with pH conditions (68–69%), and the more negative current density of the electrode at a lower pH could explain this phenomenon (CV curves in Fig. S14(d)). These results indicated that the WO<sub>3</sub>/CMK-3 cathode exhibited high H<sub>2</sub>O<sub>2</sub> production activity at different pH values, which will be a promising cathode used for H<sub>2</sub>O<sub>2</sub> production and synergistic wastewater treatment on the anode.

### 3.3. Total nitrogen removal of urine

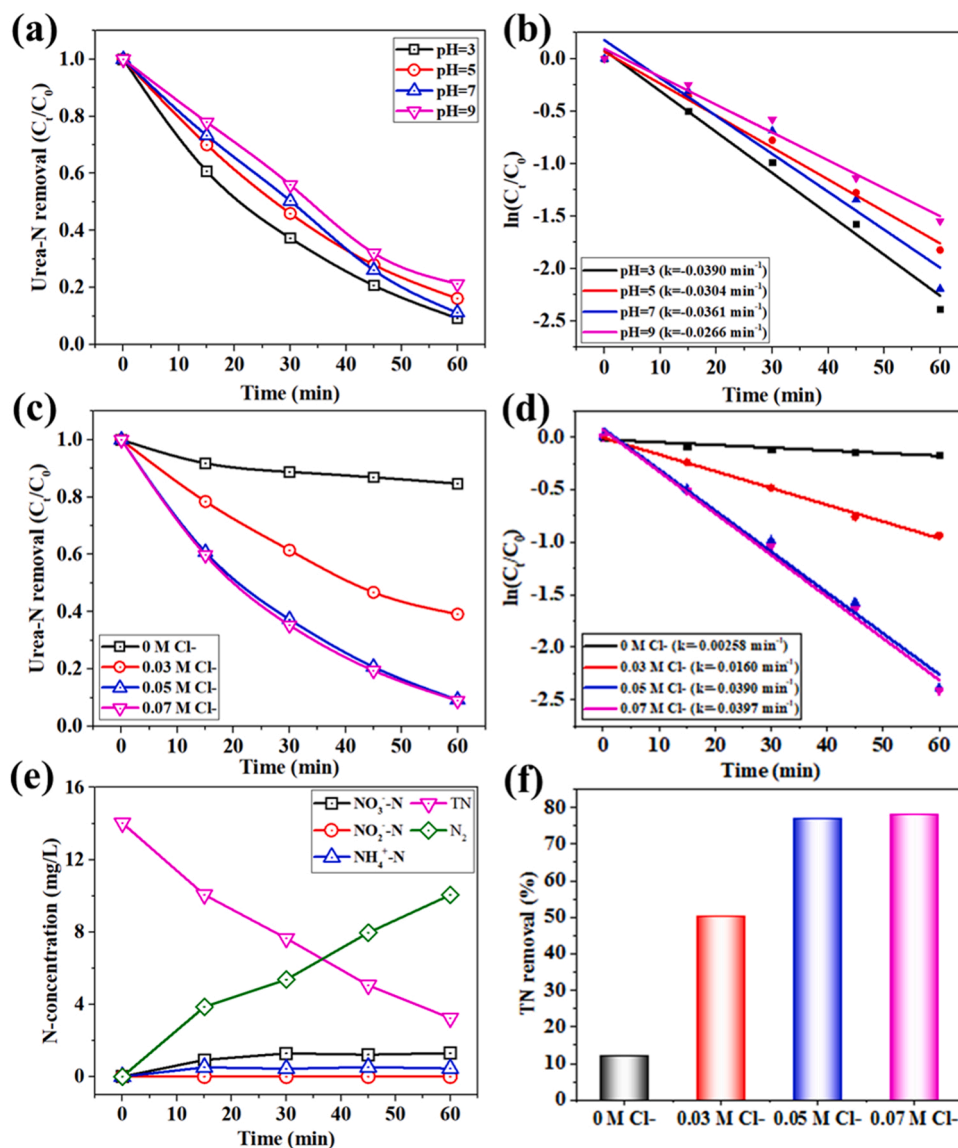
According to Eqs. (2) and 3, the urea decomposition is an exothermic process, while the reduction of oxygen to H<sub>2</sub>O<sub>2</sub> is an endothermic process, which indicates that the chemical energy released from urea decomposition may be utilized by the reaction of oxygen reduction to produce H<sub>2</sub>O<sub>2</sub> (Eq. (4)). Based on this, a novel method based on a self-biased WO<sub>3</sub>/TiO<sub>2</sub>-Si PVC photoanode and a WO<sub>3</sub>/CMK-3 cathode was proposed, which aimed at producing the high value-added chemical H<sub>2</sub>O<sub>2</sub> from efficient total nitrogen removal of urine. The mechanism of urine treatment and synergistic H<sub>2</sub>O<sub>2</sub> production was shown in Fig. S3. The Si PVC was adhered to the back of the WO<sub>3</sub>/TiO<sub>2</sub> and sealed by silicone rubber to form a self-biased composite photoanode. With a type-II interface band structure, the front WO<sub>3</sub>/TiO<sub>2</sub> photoanode can reduce the possibility of surface trap recombination and improve the separation of electron-hole pairs. Moreover, the WO<sub>3</sub>/TiO<sub>2</sub> absorbs mainly the



short-wavelength part of sunlight ( $< 460$  nm) and the filtered long-wavelength light ( $> 460$  nm) can be captured by rear Si PVC, which could simultaneously expand the absorption portion of the solar spectrum and strengthen the separation and migration of charges in the PEC system [32]. Due to the bias of Si PVC, the oxidation capacity of the  $\text{WO}_3/\text{TiO}_2$  photoanode can be greatly enhanced. The experiments of synthetic urine degradation on  $\text{WO}_3/\text{TiO}_2$ -Si PVC photoanode and synergistic  $\text{H}_2\text{O}_2$  generation on 1%  $\text{WO}_3/\text{CMK-3}$  cathode were performed. As shown in Figs. 6(a), 90.8% of urea can be removed within 60 min at pH 3. However, the TN removal rate was 78.7–88.8% when pH was 5–9. The increase of solution pH leads to decreased urea removal efficiency. At pH 3, the kinetic constant ( $k$ ) for urea degradation is  $0.0390 \text{ min}^{-1}$ , which decreases to  $0.0266 \text{ min}^{-1}$  at pH 9 (Fig. 6(b)). The pH-dependent degradation rate can be ascribed to that the lower pH of anolyte can replenish  $\text{H}^+$  for catholyte and then facilitate cathodic  $\text{H}_2\text{O}_2$  production, which in turn promote the exothermic reaction of urea decomposition. Moreover,  $\text{WO}_3/\text{TiO}_2$  seems to perform better under acidic conditions, which is responsible for the poor degradation of urea at higher pH [49].

Since the oxidation of urea at the anode is a kinetically slow process and prone to excessive oxidation to nitrate nitrogen [5,50], and the free

chlorine is considered to be the main factor in urea oxidation according to the Volmer-Heyrovsky mechanism [51], it is crucial to investigate the effect of chlorine concentration on urea degradation efficiency. Fig. 6(c) illustrated the urea removal at different initial chloride concentrations. As shown in the results, the addition of chloride remarkably boosted the removal rate of urea. The oxidation process of urea without the addition of chloride was very slow ( $15.3\%$ ). As the chloride concentration increased from  $0.03$  to  $0.07$  M, the urea degradation efficiency was significantly improved from  $60.8\%$  to  $91.0\%$ . The degradation of urea followed the pseudo-first-order kinetic principle (Fig. 6(d)), and the kinetic constant was  $0.0397 \text{ min}^{-1}$  at a  $\text{Cl}^-$  concentration of  $0.07$  M, which was  $2.5$  times than that at  $0.03$  M  $\text{Cl}^-$  ( $0.0160 \text{ min}^{-1}$ ) and  $15.4$  times than that at  $0$  M  $\text{Cl}^-$  ( $0.00258 \text{ min}^{-1}$ ). The TN removal rates of synthetic urine at different  $\text{Cl}^-$  concentrations were also monitored, and the results showed that the TN removal rate increased from  $11.9\%$  to  $78.1\%$  when  $\text{Cl}^-$  was increased from  $0$  to  $0.07$  M (Fig. 6(f)), which corresponded to the urea degradation efficiency. It is worth noting that the degradation and mineralization of urea did not increase significantly when the chloride concentration increased from  $0.05$  M to  $0.07$  M, which could be explained by the fact that higher  $\text{Cl}^-$  concentration may



**Fig. 6.** Effect of (a) anolyte pH ( $0.05 \text{ M Cl}^-$ ) and (c) initial chloride concentration ( $\text{pH}=3$ ) on the removal rate of urea in synthetic urine. (b) and (d) Corresponding plots of  $\ln(C_t/C_0)$  versus time. (e) Different N-concentrations versus time during the degradation of synthetic urine, conditions: Anolyte:  $30 \text{ mg L}^{-1}$  urea,  $0.1 \text{ M Na}_2\text{SO}_4$ ,  $0.05 \text{ M NaCl}$ ,  $\text{pH}=3$ ; Catholyte:  $\text{pH}=2$ ,  $0.1 \text{ M Na}_2\text{SO}_4$ . (f) Effects of initial chloride concentration on TN removal.

lead to the high generation of  $\text{NO}_3^-$  [52].

To determine the variation of N species in urea degradation products, we monitored the concentrations of  $\text{NO}_3\text{-N}$ ,  $\text{NO}_2\text{-N}$ ,  $\text{NH}_3\text{-N}$ , TN, and  $\text{N}_2$ , and the results were shown in Fig. 6(e). After 60 min of degradation, the concentrations of  $\text{NO}_3\text{-N}$  and  $\text{NH}_3\text{-N}$  accumulated to 1.3 and  $0.45 \text{ mg L}^{-1}$ , respectively. The  $\text{NO}_2\text{-N}$  has never been detected (below the instrument detection limit) because it can be easily oxidized in a strong oxidation environment. 76.9% of TN was removed at 60 min, indicating that the majority of the nitrogen was mineralized into the harmless  $\text{N}_2$  during the degradation of synthetic urine (71.6%), which demonstrated the excellent urine treatment capacity of the constructed PEC system.

To explore the  $\text{H}_2\text{O}_2$  production capacity of the cathode during the treatment of synthetic urine in this system, the  $\text{H}_2\text{O}_2$  yield and the Faradaic efficiency of the cathode with or without the removal of urea in the anode chamber were compared. As shown in Fig. 7(a), the cathodic  $\text{H}_2\text{O}_2$  production rate reached  $5.13 \text{ mg cm}^{-2} \text{ h}^{-1}$  in the anodic solution containing  $0.1 \text{ M Na}_2\text{SO}_4$ ,  $0.05 \text{ M NaCl}$  and  $30 \text{ mg L}^{-1}$  urea, nearly 1.34 times higher than the initial production rate ( $3.84 \text{ mg cm}^{-2} \text{ h}^{-1}$ ) in  $0.1 \text{ M Na}_2\text{SO}_4$ .

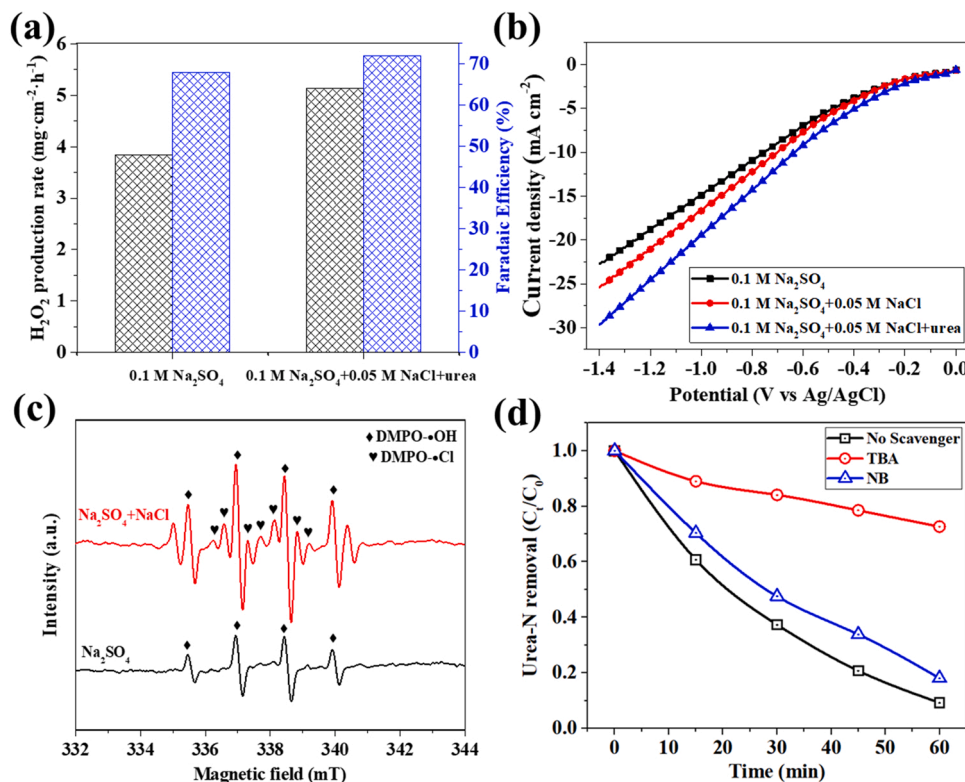
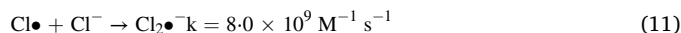
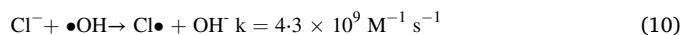
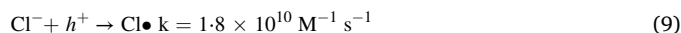
This indicated that the removal of urea had a remarkable synergistic effect on  $\text{H}_2\text{O}_2$  production, in which the potential energy released from urea degradation was recovered to form  $\text{H}_2\text{O}_2$ , and the generated electrons were efficiently captured by the cathode to participate in the oxygen reduction reaction. Moreover, several studies have also reported the feasibility of pollutant degradation to provide electrons for cathodic reduction reactions [53]. The LSV plots in Fig. 7(b) showed that the 1%  $\text{WO}_3/\text{CMK-3}$  cathode has a higher current in the presence of urea in anolyte, which corresponded to a higher urea removal rate and  $\text{H}_2\text{O}_2$  production rate.

### 3.4. Mechanisms of $\text{H}_2\text{O}_2$ production from urine treatment

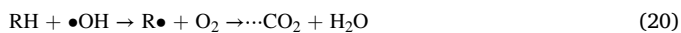
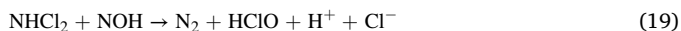
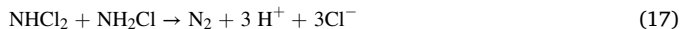
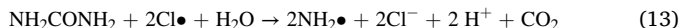
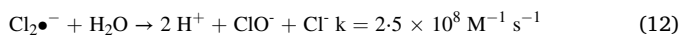
Based on the above analysis, a possible mechanism for treating urine

wastewater in the self-biased PEC system was proposed and schematically depicted in Fig. S3. To explore the existence of radicals, we investigated the radical species by electron spin resonance spectroscopy (ESR) using 5,5-dimethyl-1-pyrroline N-oxide (DMPO) as a trapping agent. The clear quartet peaks of  $\bullet\text{OH}$  with 1:2:2:1 intensity could be observed in the system without chlorine (Fig. 7(c)). When inducing  $\text{Cl}^-$  in the PEC system, seven new peaks emerged, which corresponded to the  $\text{DMPO-Cl}\bullet$  [22]. We then used different scavengers to investigate the role of  $\text{Cl}\bullet$  in urea degradation (TBA for  $\bullet\text{OH}$  and  $\text{Cl}\bullet$ , NB for  $\bullet\text{OH}$ ) [54]. As shown in Fig. 7(d), urea degradation was suppressed obviously after adding TBA, which demonstrated that  $\text{Cl}\bullet$  and  $\bullet\text{OH}$  were both involved. While urea degradation was slightly inhibited by adding NB, suggesting that the role of  $\bullet\text{OH}$  was limited. Therefore,  $\text{Cl}\bullet$ -mediated radical oxidation played a major role in urea degradation (54.6%).

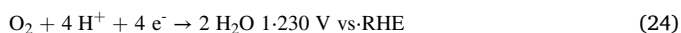
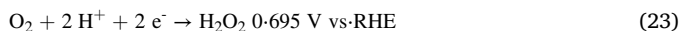
The self-bias voltage generated between the Si PVC and the  $\text{WO}_3/\text{TiO}_2$  drove the electron migration from the  $\text{WO}_3/\text{TiO}_2$  photoanode to the 1%  $\text{WO}_3/\text{CMK-3}$  cathode, effectively promoting the formation of  $\bullet\text{OH}/\text{Cl}\bullet$  on the photoanode and the production of  $\text{H}_2\text{O}_2$  on the cathode. Under light irradiation,  $\text{WO}_3/\text{TiO}_2$  photoanode generated photoexcited electron-hole pairs ( $h^+e^-$ ), and then  $h^+$  was captured by  $\text{Cl}^-$  to form  $\text{Cl}\bullet$ .  $\text{Cl}\bullet$  dominated the oxidation of urea and rapidly oxidized urea into an amine group ( $-\text{NH}_2$ ) and then converted  $\text{NH}_2\bullet$  into  $\text{N}_2$  together with  $\text{HClO}$ . Meanwhile, a cycle between  $\text{Cl}^-$  and  $\text{Cl}\bullet$  was achieved (Eqs. (13)–(19)). In addition, organic matter in urine was mineralized by  $\bullet\text{OH}$  into  $\text{CO}_2$  and  $\text{H}_2\text{O}$  (Eq. (20)) and trace amounts of the amino group were oxidized to  $\text{NO}_3^-$  (Eqs. (21) and (22)).



**Fig. 7.** (a)  $\text{H}_2\text{O}_2$  yield and Faradaic efficiency, and (b) current density of  $\text{WO}_3/\text{CMK-3}$  electrode in different systems. (c) ESR spectra during the urea removal process. (d) Related experiments of free radical quenching. Conditions: Anolyte:  $30 \text{ mg L}^{-1}$  urea,  $0.1 \text{ M Na}_2\text{SO}_4$ ,  $0.05 \text{ M NaCl}$ ,  $\text{pH} = 3$ ; Catholyte:  $\text{pH} = 2$ ,  $0.1 \text{ M Na}_2\text{SO}_4$ .



Photoelectrochemical synthesis of  $\text{H}_2\text{O}_2$  from oxygen reduction reaction (ORR) proceeds mainly via a  $2\text{e}^-$  transfer pathway (Eq. (23)) [55]. However, oxygen molecules can also be reduced to  $\text{H}_2\text{O}$  via the direct  $4\text{e}^-$  pathway (Eq. (24)). To achieve efficient  $\text{H}_2\text{O}_2$  production, seeking a highly selective cathode catalyst is necessary [56–58]. In this case, the  $\text{WO}_3$ -modified CMK-3 cathode ( $\text{WO}_3/\text{CMK-3}$ ) was prepared in this study due to its high specific surface area and hydrophilic/hydrophobic interface, which gives it a large number of catalytic active sites and efficient  $\text{O}_2$  transfer channels for efficient  $\text{H}_2\text{O}_2$  production. According to Eq. (4),  $\text{H}_2\text{O}_2$  production from urine treatment is a process with a strong thermodynamic spontaneous trend, which indicates that a feasible reversal of the thermodynamic trend of  $\text{O}_2$  reduction to  $\text{H}_2\text{O}_2$  from non-spontaneous to strong spontaneous can be achieved by combining it with a urine treatment reaction that releases large amounts of chemical energy in a photoelectrocatalytic system. Besides, the electrons generated from urine oxidation were also transferred to the  $\text{WO}_3/\text{CMK-3}$  cathode via an external circuit, which can further enhance the  $\text{H}_2\text{O}_2$  production.

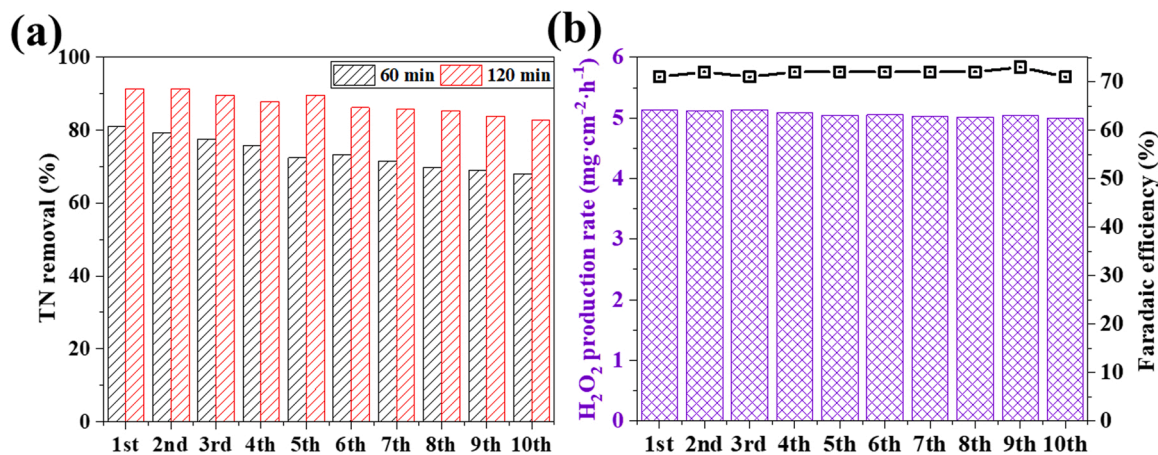


### 3.5. Actual urine treatment and cycling performance tests

To demonstrate the practicality and durability of the PEC system, experiments of actual urine treatment were performed. The actual urine samples were collected from a public latrine, which were filtered and diluted for immediate disposal. The physicochemical properties of actual urine samples were presented in Table S2. As shown in Figs. 8(a), 91.4% of TN was removed from the actual urine after 120 min of reaction. Moreover, the TN removal rate of urine samples was still as high as 82.8% after ten accumulated tests, which indicates that the  $\text{WO}_3/\text{TiO}_2$  photoanode has good treatment capability. The durability of the 1%  $\text{WO}_3/\text{CMK-3}$  cathode was also evaluated by repeated  $\text{H}_2\text{O}_2$  production experiments. In Fig. 8(b), the  $\text{H}_2\text{O}_2$  yield and Faradaic efficiency of 1%  $\text{WO}_3/\text{CMK-3}$  cathode nearly remained the same as the fresh sample after ten consecutive cycles ( $5 \text{ mg cm}^{-2} \text{ h}^{-1}$  and 71%), which demonstrates that 1%  $\text{WO}_3/\text{CMK-3}$  cathode has good stability. In addition, the morphology of the used  $\text{WO}_3/\text{TiO}_2$  photoanode and 1%  $\text{WO}_3/\text{CMK-3}$  cathode was found to be similar to that of fresh ones (Fig. S16). All these results illustrated that the fabricated PEC system possessed good durability, which had a potential for long-term application in the actual urine treatment.

## 4. Conclusions

The major sources of nitrogen pollution in wastewater treatment plants propose a great challenge for wastewater treatment. Efficient denitrification and resource utilization of urine through source separation is an effective way to mitigate urine pollution. Based on this, a novel bi-functional PEC system was constructed to realize simultaneous nitrogen removal and  $\text{H}_2\text{O}_2$  production in urine wastewater treatment. In this study, a  $\text{WO}_3/\text{TiO}_2$ -Si PVC composite photoanode was prepared to generate  $\bullet\text{OH}/\text{Cl}\bullet$  for the highly selective conversion of urine to  $\text{N}_2$  and  $\text{CO}_2$ . The chemical energy released from the denitrogenation of urine was subsequently recovered by the thermodynamically unfavorable reduction of  $\text{O}_2$  to  $\text{H}_2\text{O}_2$  on the  $\text{WO}_3/\text{CMK-3}$  cathode. Results indicated the degradation efficiency of synthetic urine within 60 min was 91.0%, and 91.4% of TN was removed from the actual urine after 120 min of reaction. The system also showed a superior performance for  $\text{H}_2\text{O}_2$  production with a yield of  $5.13 \text{ mg cm}^{-2} \text{ h}^{-1}$  in 60 min. Combined with the analysis of ESR and free radical capture experiment, it was concluded that  $\text{Cl}\bullet$  played an important role in urea oxidation. The results demonstrated that the proposed PEC system offers a foundation for the simultaneous efficient purification and resource utilization of urine.



**Fig. 8.** (a) The stability test of the  $\text{WO}_3/\text{TiO}_2$  photoanode used for TN removal of actual urine wastewater. Conditions : Anolyte: pH = 3, 0.1 M  $\text{Na}_2\text{SO}_4$  + 0.05 M NaCl; Catholyte: pH = 2, 0.1 M  $\text{Na}_2\text{SO}_4$ . (b) The stability test of the  $\text{WO}_3/\text{CMK-3}$  cathode was used for  $\text{H}_2\text{O}_2$  generation. Conditions : Anolyte: pH = 3, 0.1 M  $\text{Na}_2\text{SO}_4$  + 0.05 M NaCl, 30  $\text{mg L}^{-1}$  urea; Catholyte: pH = 2, 0.1 M  $\text{Na}_2\text{SO}_4$ .



## CRediT authorship contribution statement

**Lei Li:** Conceptualization, Data curation, Writing – original draft, Writing – review & editing. **Jinhua Li:** Visualization, Investigation, Supervision. **Fei Fang:** Investigation, Data curation. **Yan Zhang:** Investigation, Data curation, Methodology. **Tingsheng Zhou:** Methodology. **Changhui Zhou:** Methodology. **Jing Bai:** Visualization, Supervision. **Baoxue Zhou:** Conceptualization, Supervision, Project administration, Writing – review & editing.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## Data Availability

Data will be made available on request.

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## Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at [doi:10.1016/j.apcatb.2023.122776](https://doi.org/10.1016/j.apcatb.2023.122776).

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